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Flow Around a Plate at Nonzero Cavitation Numbers

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Annotation: This article discusses the issue of flow around a plate at nonzero cavitation numbers. A review is made of the difference of the cavitation numbers from zero even when flowing around the simplest outlines, which greatly complicates the mathematical analysis of the problem. The drag coefficient for the transverse flow around the plate is expressed by the same row according to the Ryabushinsky scheme. At low cavitation numbers, the Zhukovsky-Roshko scheme is considered. The formulas are given according to the Ryabushinsky scheme.

Keywords: flow, cavitation, Ryabushinsky scheme, Zhukovsky-Roshko scheme, flat cavities, cavitating body, Linear dependence, drag coefficient, lift coefficient.

The difference between the cavitation number and zero even when flowing around a body of the simplest outlines (plate) greatly complicates the mathematical analysis of the problem. We will restrict ourselves to discussing the most important results useful for understanding the physical aspects of the problem and their application to the analysis of spatial problems.

The drag coefficient for the transverse flow around the plate, calculated according to the scheme with a return stream and according to the Ryabushinsky scheme, is expressed by the same series:

$$C_x(\sigma) = \frac{2\pi}{\pi+4} \left[1 + \sigma + \frac{\sigma^2}{8(\pi+4)} + O(\sigma^3) \right] \quad (1)$$

In the case of the Zhukovsky-Roshko scheme, in the third term in brackets, the number 8 is replaced by the number 6. As you can see, for small numbers of cavitation, one can take

$$C_x(\sigma) = \frac{2\pi}{\pi+4} (1 + \sigma), \quad (2)$$

where $C_x(0) = \frac{2\pi}{\pi+4} = 0,88$.

At $\sigma = 1$ the accuracy of this approximate formula is 0.8%, and as it decreases, its accuracy increases.

Analytical behavior of the boundaries of flat cavities at $\sigma \rightarrow 0$ at large distances from the cavitating body obeys the law:

$$y - y_0 \approx C_1 \sqrt{x} + C_2 \ln x + O\left(x^{-\frac{1}{2}} \ln x\right) \quad (3)$$

Рябушинского, оцениваются формулами: The dimensions of the cavity, calculated according to the Ryabushinsky scheme, are estimated by the formulas:

a) cavity width:

$$\frac{B}{l} \approx \frac{4}{4 + \pi} \left(\frac{2 + \sigma}{\sigma} + \frac{\pi}{4} \right) \quad (4)$$

б) cavity length:

$$\frac{L}{l} \approx \frac{4}{4 + \pi} \left[\left(\frac{2 + \sigma}{\sigma} \right)^2 - \frac{1}{2} \ln 4 \frac{2 + \sigma}{\sigma} - \frac{1}{4} \right] \quad (5)$$

в) cavity lengthening:

$$\lambda = \frac{L}{B} \approx \frac{2}{\sigma} \quad (6)$$

The error in calculating the cavity width does not exceed 0.6% at $\sigma \approx 3$. Formula (5) gives overestimated results of the cavity length by 0.7% at $\sigma = 1$.

Similar numerical estimates for the configuration of cavities are obtained using other schemes.

The linear dependence of the drag coefficient on the cavitation number is also characteristic of the lift coefficient. The same pattern turns out to be valid in spatial flows. Thus, the most important role of the Kirchhoff model is emphasized, although at first glance it is unrealistic, because in reality there can be no infinite caverns.

Along with the above, it must be emphasized that the dependence $C_x(\sigma) = C_x(0)(1 + \sigma)$ well reflects the force interaction with the flow of strongly blunt bodies, the image of which was a plate installed across the flow. For pointed bodies, the linear dependence of the forces on the cavitation number is preserved, but it is more accurate to write it in the form

$$C_x(\sigma) = C_x(0)(1 + \beta\sigma) \quad (7)$$

where β — a correction factor depending on the shape of the body. Wherein $C_x(0)$, naturally also depends on the configuration of the body. A particular example is the well-known Betz formula (1931) for sharp wedges (cones):

$$C_x(\sigma) = C_x(0) + \sigma \quad (8)$$

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